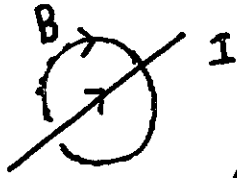


Lect: 2: Magnetic fields from steady currents

①

{ Ampere's law



$$\oint \vec{B} \cdot d\vec{l} = \frac{4\pi}{c} I$$

← we start from here to derive Biot-Savart's law

$$\oint \vec{B} \cdot d\vec{l} = \iint (\nabla \times \vec{B}) \cdot d\vec{S} = \frac{4\pi}{c} \iint \vec{j} \cdot d\vec{S}$$

\Rightarrow $\nabla \times \vec{B} = \frac{4\pi}{c} \vec{j}$ clearly Ampere's law only applies to steady-current

$$\nabla \cdot (\nabla \times \vec{B}) = \frac{4\pi}{c} \nabla \cdot \vec{j} = 0 \Rightarrow \frac{\partial \rho}{\partial t} = 0.$$

We will consider time-dependent case later.

Suppose that we know the distribution

of $\vec{j}(x, y, z)$, but it's not enough. We need to the divergence

of \vec{B} . The fact is that so far no magnetic monopole is discovered.

Any closed surface, the magnetic flux is zero $\oiint \vec{B} \cdot d\vec{S} = 0 \Rightarrow \nabla \cdot \vec{B} = 0$.

{ Vector potential

$$\nabla \cdot \vec{B} = 0 \Rightarrow \vec{B} = \nabla \times \vec{A}$$

\vec{A} is well-defined up to $\vec{A} + \nabla f$

$$\nabla \times \vec{B} = \nabla \times (\nabla \times \vec{A}) = \frac{4\pi}{c} \vec{j}$$

$$\nabla \times (\nabla \times \vec{A}) = \nabla (\nabla \cdot \vec{A}) - \nabla^2 \vec{A} = \frac{4\pi}{c} \vec{j}$$

we further impose the condition $\nabla \cdot \vec{A} = 0 \Rightarrow$

$$\nabla^2 \vec{A} = -\frac{4\pi}{c} \vec{j}$$

$$\nabla \cdot \vec{A} = 0$$

Assuming \vec{J} goes to zero at infinity, we can read off from the

Solution of Poisson equation:

$$\vec{A}(\vec{r}) = \frac{1}{c} \iiint \frac{\vec{j}(\vec{r}') d^3r'}{|\vec{r} - \vec{r}'|}$$

$$\begin{aligned} \text{check } \nabla \cdot \vec{A}(\vec{r}) = 0. \Rightarrow \nabla \cdot \vec{A}(\vec{r}) &= \frac{1}{c} \iiint \vec{j}(\vec{r}') \nabla_r \frac{1}{|\vec{r} - \vec{r}'|} d^3r' \\ &= -\frac{1}{c} \iiint \vec{j}(\vec{r}') \nabla_{r'} \frac{1}{|\vec{r} - \vec{r}'|} d^3r' \\ &= -\frac{1}{c} \iiint \left[\nabla_{r'} \left[\frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} \right] - (\nabla' \cdot \vec{j}(\vec{r}')) \frac{1}{|\vec{r} - \vec{r}'|} \right] d^3r' \end{aligned}$$

$$\nabla \cdot \vec{A}(\vec{r}) = -\frac{1}{c} \oint \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|} \cdot d\vec{s}' = 0 \leftarrow \begin{array}{l} \text{assuming } j(r) \rightarrow 0 \\ \text{at } r \rightarrow +\infty, \text{ or boundary} \end{array}$$

Example: 2D, E and B duality:

Assume an 2D distribution $j_z(x, y)$, which does not depend on z .
we cannot use the above formula because, j_z extends to $z = \pm\infty$.

B only has in-plane component. define $\vec{E} = \vec{B} \times \hat{z}$, and $\vec{A} = \varphi(x, y) \hat{z}$

$$\Rightarrow \nabla \times \vec{A} = \nabla \times (\varphi(x, y) \hat{z}) = (\nabla \cdot \varphi) \times \hat{z} = \vec{B}$$

$$[(\nabla \cdot \varphi) \times \hat{z}] \times \hat{z} = \vec{B} \times \hat{z}$$

$$\boxed{-\nabla \varphi = \vec{E} = \vec{B} \times \hat{z}} \Rightarrow -\nabla^2 \varphi = \nabla \cdot (\vec{B} \times \hat{z}) = \hat{z} \cdot \nabla \times \vec{B} = j_z(x, y)$$

so we transform it to an electro-static problem.

$$\vec{B}(r) = \frac{I}{c} \oint \frac{d\vec{\ell} \times \vec{r}}{r^2}$$

$$\Rightarrow d\vec{B}(r) = -\frac{I}{c} \frac{d\vec{\ell} \times \nabla_r \frac{1}{|\vec{r}-\vec{r}'|}}{|\vec{r}-\vec{r}'|^3} = -\frac{I}{c} d\vec{\ell} \times \left(-\frac{(\vec{r}-\vec{r}')}{|\vec{r}-\vec{r}'|^3} \right)$$

$$= \frac{I}{c r^2} d\vec{\ell} \times \vec{r} \quad \text{where } \vec{r} = \frac{\vec{r}-\vec{r}'}{|\vec{r}-\vec{r}'|}$$

$d\vec{\ell}$ is a const vector respect to ∇_r

$$d\vec{B}(r) = \nabla \times d\vec{A}(r) = \frac{I}{c} \nabla \times \left(\frac{d\vec{\ell}}{|\vec{r}-\vec{r}'|} \right) = \frac{I}{c} \left(-d\vec{\ell} \times \nabla \frac{1}{|\vec{r}-\vec{r}'|} \right)$$

$$d\vec{A}(r) = \frac{I}{c} \frac{d\vec{\ell}}{|\vec{r}-\vec{r}'|}$$

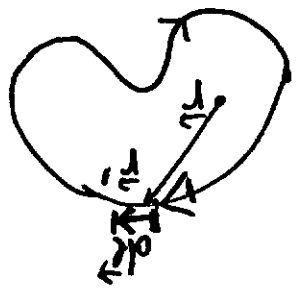
thus the contribution to \vec{B} from this line segment is

$$\Rightarrow \vec{A}(r) = \frac{I}{c} \int \frac{d\vec{\ell}}{|\vec{r}-\vec{r}'|}, \quad \text{we will find here } \Rightarrow \text{Biot-Savart law.}$$

$$\Rightarrow \vec{j} d\vec{r}' = I d\vec{\ell}$$

$$j = \frac{I}{a} \quad a: \text{cross section of wire}$$

$$d^3r' = a d\ell$$



Magnetic fields from a general shape of wire

short range cut off

$$\varphi(r) = \frac{I}{c} \int \frac{d\ell}{r} \Rightarrow \varphi(r) = -\frac{I}{c} \ln r$$

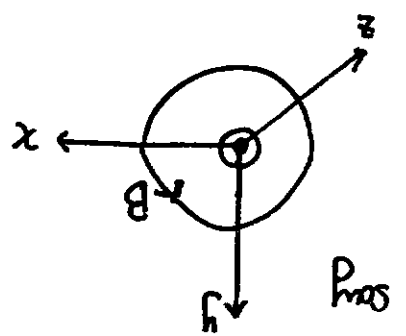
$$= -\frac{I}{c} \ln \sqrt{x^2 + y^2} = -\frac{I}{2c} \ln(x^2 + y^2)$$

$$\vec{E} = -\nabla \varphi \Rightarrow \frac{\partial \varphi}{\partial x} = -\frac{I}{c} \frac{x}{x^2 + y^2} = \frac{I}{2c} \frac{x}{r^2}$$

$$\frac{\partial \varphi}{\partial y} = -\frac{I}{c} \frac{y}{x^2 + y^2} = \frac{I}{2c} \frac{y}{r^2}$$

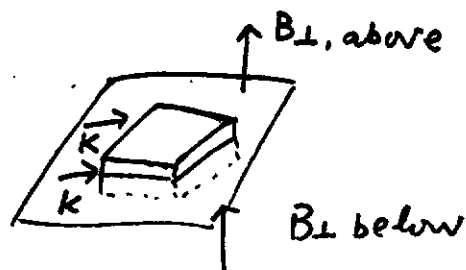
$$\vec{B} = \frac{2I}{c r} \vec{e}_\varphi = \frac{2I}{c} \frac{1}{r} \begin{pmatrix} -y \\ x \\ 0 \end{pmatrix}$$

$$\vec{j} = \delta(r) \vec{e}_z$$



§ magneto-static boundary condition

When there's surface current K , magnetic fields can be discontinuous.



But the norm component remains continuous.

$$\oint \vec{B} \cdot d\vec{S} = 0 \Rightarrow (B_{\perp, \text{above}} - B_{\perp, \text{below}}) \cdot S = 0 \Rightarrow \boxed{B_{\perp, \text{above}} = B_{\perp, \text{below}}}$$

$$\oint \vec{B} \cdot d\vec{l} = \frac{4\pi}{c} \vec{K} \cdot d\vec{l}$$

$$\Rightarrow (\vec{B}''_{\text{above}} - \vec{B}''_{\text{below}}) \cdot \Delta\vec{l} = \frac{4\pi}{c} \vec{K} \cdot (\hat{n} \times \Delta\vec{l})$$

$$= \frac{4\pi}{c} \Delta\vec{l} \cdot (\vec{K} \times \hat{n})$$

$$\Rightarrow \boxed{\vec{B}''_{\text{above}} - \vec{B}''_{\text{below}} = \frac{4\pi}{c} \vec{K} \times \hat{n}}$$



We may also need boundary conditions for vector potential A . Since A satisfies 2nd differential Eq, its discontinuity appears at its derivative. \vec{A} itself is continuous.

$$\nabla \cdot \vec{A} = 0 \Rightarrow \text{the normal component of } A \text{ is continuous}$$

$$\oint \vec{A} \cdot d\vec{l} = \dots \rightarrow 0 \text{ as the thickness of } \Delta h \rightarrow 0 \text{ if } B \text{ is regular.}$$

set the triad frame $e_{\hat{n}}$, $e_{\hat{k}}$, and $e_{\hat{k} \times \hat{n}}$.

$$\vec{B} \cdot e_{\hat{k} \times \hat{n}} = -\partial_n A_{\hat{k}} + \partial_{\hat{k}} A_{\hat{n}}, \text{ only this component of } B \text{ is discontinuous}$$

we don't expect discontinuity of $\partial_{\hat{k}} A_{\hat{n}}$, because $A_{\hat{n}}$ is continuous and \hat{k} is parallel to the boundary. The discontinuity comes from $\partial_n A_{\hat{k}}$.

$$\Rightarrow (\partial_n A_{\hat{k}})_{\text{above}} - (\partial_n A_{\hat{k}})_{\text{below}} = -\frac{4\pi}{c} K$$

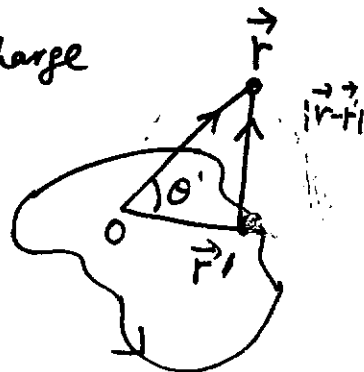
$$\text{or } (\partial_n \vec{A})_{\text{above}} - (\partial_n \vec{A})_{\text{below}} = -\frac{4\pi}{c} \vec{K}$$

in comparison: boundary condition for electric surface charge

$$(\vec{E}_{||})_{\text{above}} = (\vec{E}_{||})_{\text{below}}$$

$$(\vec{E} \cdot \hat{n})_{\text{above}} - (\vec{E} \cdot \hat{n})_{\text{below}} = 4\pi\sigma$$

$$\text{or } -\left(\frac{\partial\phi}{\partial n}\right)_{\text{above}} + \left(\frac{\partial\phi}{\partial n}\right)_{\text{below}} = 4\pi\sigma$$



§ Multiple expansion of the vector potential

we need to use

$$\frac{1}{|\vec{r}-\vec{r}'|} = \frac{1}{\sqrt{r^2 + r'^2 - 2rr'\cos\theta'}} = \frac{1}{r} \sum_{n=0}^{\infty} \left(\frac{r'}{r}\right)^n P_n(\cos\theta')$$

$$\vec{A}(\vec{r}) = \frac{I}{c} \oint \frac{d\vec{l}'}{|\vec{r}-\vec{r}'|} = \frac{I}{c} \sum_{n=0}^{\infty} \frac{1}{r^{n+1}} \oint (r')^n P_n(\cos\theta') d\vec{l}'$$

$$= \frac{I}{c} \left[\underbrace{\frac{1}{r} \oint d\vec{l}'}_{\text{monopole} = 0} + \frac{1}{r^2} \underbrace{\oint r' \cos\theta' d\vec{l}'}_{\text{dipole}} + \frac{1}{r^3} \underbrace{\oint r'^2 \left(\frac{3}{2} \cos^2\theta' - \frac{1}{2}\right) d\vec{l}'}_{\text{quadrupole}} + \dots \right]$$

The magnetic dipole component

$$\vec{A}_{\text{dip}}(\vec{r}) = \frac{I}{cr^2} \oint r' \cos\theta' d\vec{l}' = \frac{I}{cr^2} \oint (\hat{r} \cdot \vec{r}') d\vec{l}'$$

using the identity $\oint (\vec{c} \cdot \vec{r}) d\vec{l}' = \vec{a} \times \vec{c}$, where \vec{c} is a const vector
 $\vec{a} = \frac{1}{2} \oint \vec{r}' \times d\vec{l}'$

$$\oint (\hat{r} \cdot \vec{r}') d\vec{l}' = \vec{a} \times \hat{r} = \left[\frac{1}{2} \oint \vec{r}' \times d\vec{l}' \right] \times \hat{r}$$

$$\Rightarrow \vec{A}_{dip}(\vec{r}) = \frac{1}{c} \frac{\vec{m} \times \hat{r}}{r^2}, \text{ where } m = \frac{1}{2} \oint \vec{r}' \times d\vec{l}'$$

where $\vec{a} = \oint \vec{r}' \times d\vec{l}'$ is the vector area of a surface, which is determined by the boundary. (C.f. Prob 1-61).

field from a dipole.

$$\vec{B}_{dip}(\vec{r}) = \nabla \times \vec{A}_{dip}(\vec{r}) = \frac{1}{c} \nabla \times \left(\frac{\vec{m} \times \hat{r}}{r^2} \right)$$

using $\nabla \times (\vec{A} \times \vec{B}) = (\vec{B} \cdot \nabla) \vec{A} - (\vec{A} \cdot \nabla) \vec{B} + \vec{A} (\nabla \cdot \vec{B}) - \vec{B} (\nabla \cdot \vec{A})$

$$\nabla \times \left(\vec{m} \times \frac{\hat{r}}{r^2} \right) = -(\vec{m} \cdot \nabla) \left(\frac{\hat{r}}{r^2} \right) + \vec{m} \left(\nabla \cdot \frac{\hat{r}}{r^2} \right) \leftarrow \boxed{\vec{m} \cdot 4\pi \delta(\vec{r})}$$

singular point at origin, neglected!

$$\nabla (\vec{A} \cdot \vec{B}) = \vec{A} \times (\nabla \times \vec{B}) + \vec{B} \times (\nabla \times \vec{A}) + (\vec{A} \cdot \nabla) \vec{B} + (\vec{B} \cdot \nabla) \vec{A} \Rightarrow$$

$$\Rightarrow \nabla \left(\frac{\vec{m} \cdot \hat{r}}{r^2} \right) = \vec{m} \cdot \nabla \frac{\hat{r}}{r^2}$$

$$\Rightarrow \nabla \times \left(\vec{m} \times \frac{\hat{r}}{r^2} \right) = - \nabla \left(\frac{\vec{m} \cdot \hat{r}}{r^2} \right) = -(\vec{m} \cdot \nabla) \frac{\hat{r}}{r^2} - \nabla (\vec{m} \cdot \hat{r}) \frac{1}{r^3}$$

$$\nabla \frac{1}{r^3} = \frac{-3 \hat{r}}{r^4} \quad \nabla (\vec{m} \cdot \hat{r}) = \vec{m}$$

$$\Rightarrow \nabla \times \left(\vec{m} \times \frac{\hat{r}}{r^2} \right) = \frac{3(\vec{m} \cdot \hat{r}) \hat{r}}{r^3} - \frac{\vec{m}}{r^3}$$

$$\Rightarrow \vec{B}_{dip}(\vec{r}) = \frac{1}{c} \left(\frac{3(\vec{m} \cdot \hat{r}) \hat{r} - \vec{m}}{r^3} \right)$$

The interaction energy between two magnetic dipoles

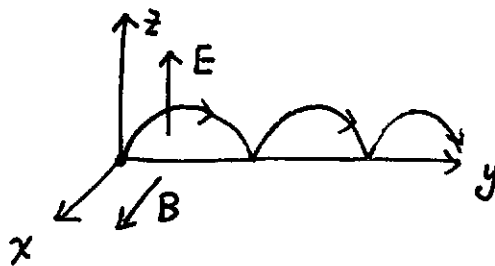
$$V = -\vec{B}_{12} \cdot \vec{m}_2 = \frac{1}{c} \frac{1}{r^3} \left[\vec{m}_1 \cdot \vec{m}_2 - 3(\vec{m}_1 \cdot \hat{r})(\vec{m}_2 \cdot \hat{r}) \right]$$

Lect 3: Examples of magnetic fields

①

Griffiths Ex 5.2:

related to the classic picture of quantum Hall edge states



Solution: no force in the x-direction. The motion is in the yz-plane.

$$\vec{r}(t) = (0, y(t), z(t))$$

$$\vec{F}_L = q\vec{v} \times \vec{B} = \frac{qB}{c} (\dot{z}\hat{y} - \dot{y}\hat{z}), \quad \vec{F}_E = qE\hat{z}$$

$$\Rightarrow q\left(E - \frac{B}{c}\dot{y}\right)\hat{z} + \frac{qB}{c}\dot{z}\hat{y} = m\ddot{y}\hat{y} + \ddot{z}\hat{z}$$

$$\Rightarrow \frac{qB\dot{z}}{c} = m\ddot{y}$$

define $\omega = \frac{qB}{mc}$, ← cyclotron frequency

$$\begin{cases} qE - \frac{qB}{c}\dot{y} = m\ddot{z} \end{cases}$$

$$\Rightarrow \begin{cases} \ddot{y} = \omega\dot{z} \\ \ddot{z} = \omega\left(\frac{EC}{B} - \dot{y}\right) \end{cases}$$

$$\Rightarrow \ddot{z} = -\omega\dot{y} = -\omega^2 z$$

$$\Rightarrow \dot{z} = A\cos\omega t + B\sin\omega t$$

$$\Rightarrow z = \frac{C_1\cos\omega t + C_2\sin\omega t + C_3}{\omega}$$

$$\ddot{z} = -\omega^2[C_1\cos\omega t + C_2\sin\omega t]$$

$$\Rightarrow \dot{y} = -\frac{\dot{z}}{\omega} + \frac{EC}{B} = \omega[C_1\sin\omega t + C_2\cos\omega t] + \frac{EC}{B}$$

$$\Rightarrow \underline{y = C_1\sin\omega t - C_2\cos\omega t + \frac{EC}{B}t + C_4}$$

plug into the initial condition $y(0) = z(0) = \dot{y}(0) = \dot{z}(0) = 0$

$$\Rightarrow \begin{cases} y(t) = \frac{EC}{\omega B}(\omega t - \sin\omega t) \\ z(t) = \frac{EC}{\omega B}(1 - \cos\omega t) \end{cases}$$

define $R = \frac{EC}{B\omega}$ radius

$$\Rightarrow (y - \underbrace{R\omega t}_v t)^2 + (z - R)^2 = R^2$$

Cycloid

$$\boxed{v = \frac{EC}{B}}$$

2: Start from Biot-Savart law to prove $\nabla \cdot \vec{B} = 0$.

$$\vec{B}(\vec{r}) = \frac{c}{4\pi} \int \frac{\vec{j}(\vec{r}') \times \hat{r}_{12}}{r_{12}^2} d^3r'$$

$$\nabla \cdot \vec{B}(\vec{r}) = \frac{c}{4\pi} \int \nabla_r \cdot \left[\frac{\vec{j}(\vec{r}') \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} \right] d^3r'$$

$$= \frac{c}{4\pi} \int \vec{j}(\vec{r}') \cdot \left[\nabla_r \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right] d^3r' = 0$$

$$\nabla \times \vec{B}(\vec{r}) = \frac{c}{4\pi} \int \nabla_r \times \left[\frac{\vec{j}(\vec{r}') \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} \right] d^3r'$$

$$\nabla \times \left(\vec{j}(\vec{r}') \times \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) = \vec{j}(\vec{r}') \left(\nabla_r \cdot \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) - \left(\vec{j}(\vec{r}') \cdot \nabla_r \right) \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3}$$

The second term $-\vec{j}(\vec{r}') \cdot \nabla_r \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} = \left(\vec{j}(\vec{r}') \cdot \nabla_{r'} \right) \left(\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) = \nabla_{r'} \cdot \left(\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \vec{j}(\vec{r}') \right)$
 ← total derivative

~~using $\nabla \cdot (\vec{A} \times \vec{B}) = \vec{B} \cdot (\nabla \times \vec{A}) - \vec{A} \cdot (\nabla \times \vec{B})$~~
 $-\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \cdot \nabla_{r'} \vec{j}(\vec{r}') = 0$

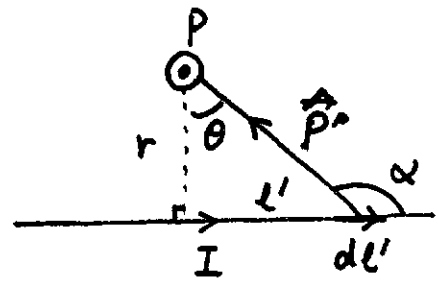
⇒ the second term vanishes after volume integral

$$\Rightarrow \nabla \times \vec{B}(\vec{r}) = \frac{c}{4\pi} \int \frac{\vec{j}(\vec{r}')}{|\vec{r} - \vec{r}'|^3} \nabla_r \cdot \left(\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) d^3r' = \frac{c}{4\pi} \int \vec{j}(\vec{r}') \delta(\vec{r} - \vec{r}') d^3r' = \frac{c}{4\pi} \vec{j}(\vec{r})$$



3: Application of Biot-Savart law

§ B-field from a long straight line:



$d\vec{l}' \times \hat{p}$ points out of page, with the

magnitude $dl' \sin \alpha = dl' \cos \theta$. $l' = r \tan \theta \Rightarrow dl' = r \sec^2 \theta d\theta$

$$p^2 = \frac{r^2}{\cos^2 \theta} \Rightarrow B = \frac{I}{c} \int \frac{d\vec{l}' \times \hat{p}}{p^2}$$

$$B = \frac{I}{c} \int_{-\pi/2}^{\pi/2} \frac{r \sec^2 \theta \cos \theta d\theta}{r^2 / \cos^2 \theta} = \frac{I}{cr} \int_{-\pi/2}^{\pi/2} \cos \theta d\theta = \frac{I}{cr} \sin \theta \Big|_{-\pi/2}^{\pi/2} = \frac{2I}{cr}$$

The force between two parallel wire $\vec{F} = \int (\frac{\vec{v}}{c} \times \vec{B}) dq = \int (\frac{\vec{v}}{c} \times \vec{B}) \lambda dl$

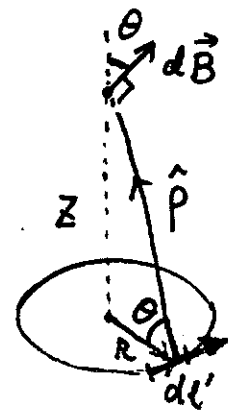
$$\Rightarrow \vec{F} = \int (\vec{I} \times \vec{B}) \frac{dl}{c} \Rightarrow \boxed{\frac{F}{l} = \frac{2I_1 I_2}{c^2 d}}$$

§: B-field at distance z above the center of a circular loop of radius R with a steady current I .

$d\vec{l}' \times \hat{p}$ has the magnitude dl' , its direction as plotted forming a polar angle θ with the z -axis.

$$\Rightarrow B_z = \frac{I}{c} \int \frac{dl' \cos \theta}{p^3} = \frac{I \cos \theta}{p^3 c} \cdot 2\pi R = \frac{2\pi I}{c} \frac{R^2}{p^3}$$

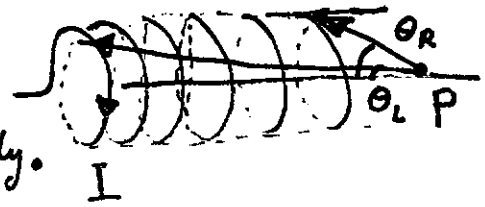
$$= \frac{2\pi I}{c} \frac{R^2}{(R^2 + z^2)^{3/2}} \quad \text{or} \quad \boxed{B_z = \frac{2\pi I \cos^3 \theta}{cR}}$$



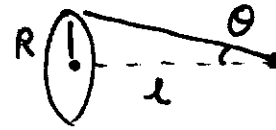
Other components average to zero.

§ B-field at axis of a wound solenoid

Suppose that the left and right ends span the polar angles of θ_L and θ_R , respectively.



$$dB = \frac{2\pi\lambda dl}{CR} \sin^3\theta = \frac{2\pi\lambda}{CR} \sin\theta d\theta$$



$$B = \int_{\theta_L}^{\theta_R} dB = -\frac{2\pi\lambda}{CR} R \cos\theta \Big|_{\theta_L}^{\theta_R} = \frac{2\pi\lambda}{C} [\cos\theta_L - \cos\theta_R]$$

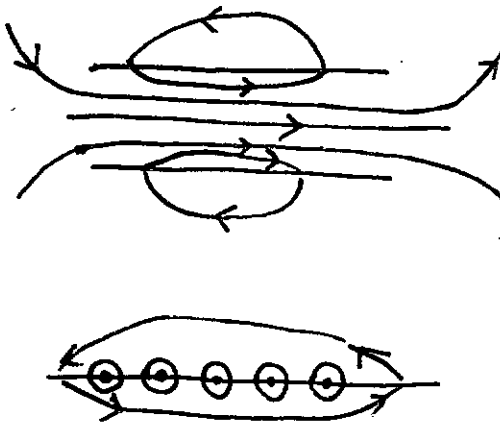
$$l = R \cot\theta$$

$$dl = -R \csc^2\theta d\theta$$

for an infinitely long solenoid,

$$\theta_L = 0, \theta_R = \pi \Rightarrow B = \frac{4\pi\lambda}{C}$$

where $\lambda = I \cdot n$, and n is the num of turns per length.



B-field of a solenoid.

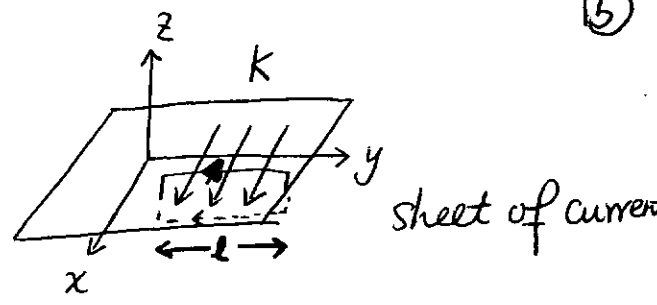
4: Application of Ampere's law + symmetric analysis

① B can only along "circumferential" direction. 

$$\oint B \cdot dl = \frac{4\pi I}{c} \Rightarrow B \cdot 2\pi r = \frac{4\pi I}{c} \Rightarrow B = \frac{2I}{cr}$$

* B-field from a sheet-current.

B should have translational symmetry, i.e. B is uniform along xy-direction.



① Can B has a z-component?

no. The system has the symmetry of Combined time-reversal and rotation along z-axis 180° .

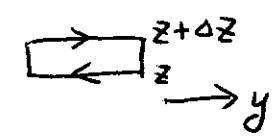
This operations flip the direction of B_z . So B can only be in the plane.

② The system has the symmetry of time-reversal and reflectional respect to xy plane.

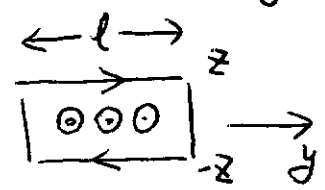
B is an axial vector $\Rightarrow B_x \xrightarrow{TR} -B_x \xrightarrow{Ref} -B_x$. Thus $B_x = 0$.

③ B can only along y-direction. B_y should not depend on z. for $z > 0$

Let us choose a loop at $z > 0 \Rightarrow B_y(z) = B_y(z + \Delta z)$.



for a loop crossing the current sheet.



~~$B_y = 2l$~~

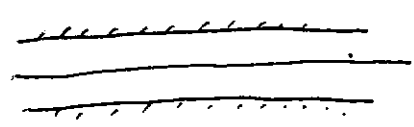
The system has rotation symmetry around x-axis at 180°

$$\Rightarrow B_y(z) = -B_y(-z) \Rightarrow B_y(z) \cdot 2 \cdot l = -\frac{4\pi}{c} K \cdot l$$

$$\Rightarrow B_y(z) = \begin{cases} -\frac{2\pi}{c} K & \text{for } z > 0 \\ \frac{2\pi}{c} K & \text{for } z < 0 \end{cases}$$

* B-field from an infinitely long solenoid

The system has rotational symmetry around



the axis.

① B cannot have radial component, otherwise $\oint B \cdot ds \neq 0$.

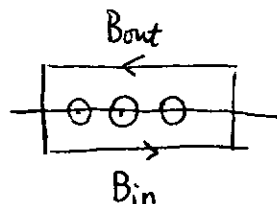
② B cannot have "circumferential" component, otherwise $\oint \vec{B} \cdot d\vec{l} \neq 0$. ⑥

③ B can only be along axial. It can also be proved that B is uniform inside the solenoid, and outside.

$$(B_{in} - B_{out}) \cdot l = \frac{4\pi}{c} I N$$

$$B_{out} = 0 \text{ if we set } r \rightarrow \infty$$

$$\Rightarrow B_{in} = \frac{4\pi}{c} I n \text{ along axis.}$$



★: a toroidal coil of a circular ring (actually can be any shape). The winding is uniform. What's the distribution of B-field?

we first use Biot-Savart law to prove that B is only circumferential. This can also be proved simply by symmetry.

Our system has rotational symmetry around "z"-axis, without loss of generality, let us consider a point r in the xz-plane, with $\vec{r} = (x, 0, z)$

the coordinate of r' on the toroidal coil

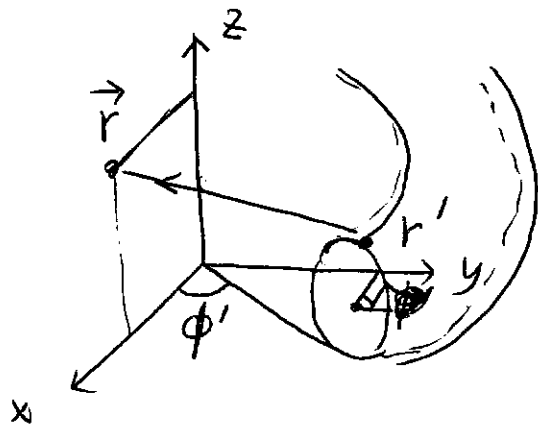
$$\vec{r}' = (s' \cos \phi', s' \sin \phi', z')$$

azimuthal angle.

the current I has no ϕ dependence

$$\vec{I} = (I_s \cos \phi', I_s \sin \phi', I_z)$$

$$\Rightarrow d\vec{B} = \frac{1}{c} \frac{\vec{I} \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} dl'$$



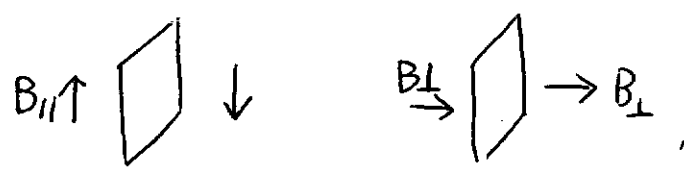
$$\vec{I} \times (\vec{r} - \vec{r}') = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ I_s \cos\phi' & I_s \sin\phi' & I_z \\ x - S' \cos\phi' & -S' \sin\phi' & z - z' \end{vmatrix} = \sin\phi' (I_s(z-z') + S'I_z) \hat{x} + [I_z(x - S' \cos\phi') - I_s \cos\phi' (z-z')] \hat{y} + [-I_s x \sin\phi'] \hat{z}$$

the contribution to \hat{x} and \hat{z} are odd functions of ϕ' \Rightarrow ^{vanishes} after integration

$\Rightarrow d\vec{B}$ only along the \hat{y} -direction. or \vec{B} is along 'circumferential'.

or we can simply get it from symmetry analysis.

\vec{B} is axial-vector. It has different properties under reflection operation.



Can you explain why?

~~Our system has reflection symmetry~~

Our system has reflection symmetry respect to any vertical plane $\Rightarrow B$ cannot be parallel to that plane. B can only be perpendicular to the vertical-radial plane. $\Rightarrow B$ is circumferential.

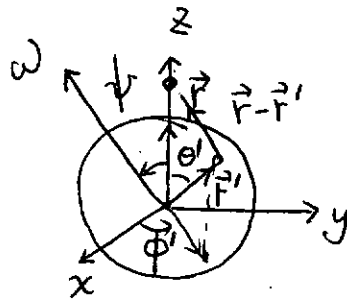
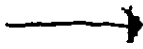
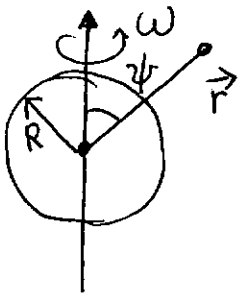
Then the results are straight-forward. For point \vec{r} inside the torus

with radius ρ to the z-axis

~~$$B(\rho) = 2\pi \rho = \frac{4\pi}{c} I \cdot N \Rightarrow B(\rho) = \frac{2IN}{\rho c}$$~~

$$B(\rho) = \frac{2I}{c} \frac{N}{\rho}, \text{ otherwise } B(\rho) = 0.$$

§ Magnetic field of a rotating spherical shell



we rotate \vec{r} to the z-axis, and $\vec{\omega}$ in the x-z plane. \vec{r}' is on the sphere with (θ', ϕ')

$$\vec{A}(\vec{r}) = \frac{1}{c} \int \frac{\vec{K}(\vec{r}')}{|\vec{r} - \vec{r}'|} da'$$

where $\vec{K}(\vec{r}') = \sigma \vec{v}$

$$|\vec{r} - \vec{r}'| = \sqrt{R^2 + r^2 - 2Rr \cos \theta'}$$

$$da' = R^2 \sin \theta' d\theta' d\phi'$$

$$\vec{v} = \vec{\omega} \times \vec{r}' = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \omega \sin \psi & 0 & \omega \cos \psi \\ R \sin \theta' \cos \phi' & R \sin \theta' \sin \phi' & R \cos \theta' \end{vmatrix}$$

$$= R\omega [-\cos \psi \sin \theta' \sin \phi' \hat{x} + (\cos \psi \sin \theta' \cos \phi' - \sin \psi \cos \theta') \hat{y} + \sin \psi \sin \theta' \sin \phi' \hat{z}]$$

these terms contains $\cos \phi'$ & $\sin \phi'$ go to zero after average over ϕ'

\Rightarrow only $A_y(\vec{r}) \neq 0$. $-\hat{y}$ is the direction of $\vec{\omega} \times \vec{r}$.

$$\Rightarrow \vec{A}(\vec{r}) = \frac{1}{c} \int \frac{\sigma \vec{v}}{|\vec{r} - \vec{r}'|} da' = \frac{2\pi R^3 \sigma \omega \sin \psi}{c} \int_0^\pi \frac{\cos \theta' d\theta'}{\sqrt{R^2 + r^2 - 2Rr \cos \theta'}}$$

$$\int_{-1}^1 \frac{u du}{\sqrt{R^2 + r^2 - 2Rru}} = - \frac{R^2 + r^2 + Rru}{3R^2 r^2} \sqrt{R^2 + r^2 - 2Rru} \Big|_{-1}^{+1} =$$

$$= - \frac{1}{3R^2 r^2} [(R^2 + r^2 + Rr) |R-r| - (R^2 + r^2 - Rr)(R+r)]$$

$$= \begin{cases} \frac{2r}{3R^2} & (R > r) \\ \frac{2R}{3r^2} & (R < r) \end{cases}$$

remember $\vec{\omega} \times \vec{r} = -\omega r \sin \psi \hat{y}$

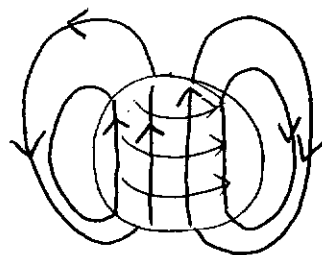
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$$\Rightarrow \vec{A}(r) = \frac{4\pi}{3c} R\sigma (\vec{\omega} \times \vec{r}) \quad \text{if } r \text{ is inside sphere}$$

$$\left\{ \begin{array}{l} \frac{4\pi}{3c} \frac{R^4 \sigma}{r^3} (\vec{\omega} \times \vec{r}) \quad \text{if } r \text{ is outside sphere} \end{array} \right.$$

if set back $\vec{\omega}$ along z-axis \Rightarrow

$$A(r, \theta, \varphi) = \begin{cases} \frac{4\pi}{3c} R\omega\sigma r \sin\theta \hat{e}_\varphi & (r \leq R) \\ \frac{4\pi}{3c} \frac{R^4}{r^2} \omega\sigma \sin\theta \hat{e}_\varphi & (r \geq R) \end{cases}$$



$$\vec{B} = \nabla \times \vec{A}(r)$$

$$\nabla \times (\vec{\omega} \times \vec{r}) = -(\underbrace{\vec{\omega} \cdot \nabla}_{\vec{\omega}}) \vec{r} + \vec{\omega} (\nabla \cdot \vec{r}) = 2\vec{\omega}$$

$$\Rightarrow \vec{B}_{\text{inside}} = \frac{8\pi}{3c} R\sigma \vec{\omega}$$

$$\nabla \times (\vec{\omega} \times \frac{\hat{r}}{r^2}) = -(\vec{\omega} \cdot \nabla) (\frac{\hat{r}}{r^2}) + \vec{\omega} (\nabla \cdot \frac{\hat{r}}{r^2})$$

$$= -\nabla \left(\frac{\vec{\omega} \cdot \hat{r}}{r^2} \right) + \vec{\omega} 4\pi \delta(r) \quad \leftarrow \text{go to zero, because } |\vec{r}| > R$$

$$\nabla \left(\frac{\vec{\omega} \cdot \hat{r}}{r^3} \right) = -(\vec{\omega} \cdot \hat{r}) \nabla \frac{1}{r^3} - \nabla (\vec{\omega} \cdot \hat{r}) \frac{1}{r^3}$$

$$\nabla \times (\vec{\omega} \times \frac{\hat{r}}{r^2}) = \frac{3(\vec{\omega} \cdot \hat{r}) \hat{r}}{r^3} - \frac{\vec{\omega}}{r^3}$$

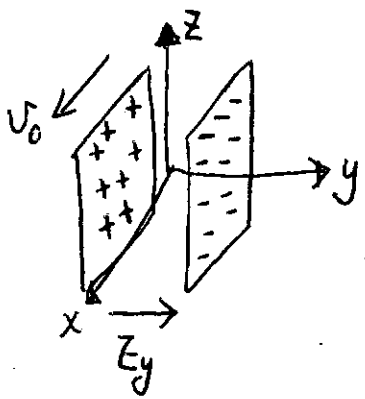
$$\vec{B}_{\text{outside}} = \frac{4\pi}{3c} R^4 \sigma \left[\frac{3(\vec{\omega} \cdot \hat{r}) \hat{r}}{r^3} - \frac{\vec{\omega}}{r^3} \right] \quad \text{its a dipolar field}$$

$$\text{with } \vec{m} = \frac{4\pi}{3c} R^4 \sigma \vec{\omega}$$

Lect 4: Transformation of E-M fields

in Frame F

Let us consider two plates in the xz-plane. The surface charge density $\pm \sigma$

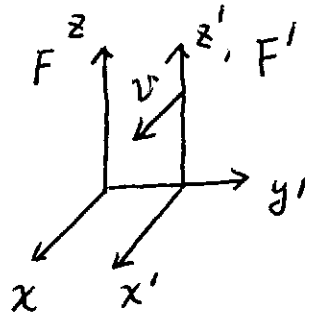


$$E_y = 4\pi\sigma.$$

The two plates move along x-direction at the speed v_0

$$\Rightarrow J_x = \sigma v_0, \text{ thus } B_z = \frac{4\pi J_x}{c} = \frac{4\pi\sigma v_0}{c}.$$

we consider another frame F' , which moves on the speed v along x-axis respect with F , what the fields observed in F' ?



In F' , the velocity of the two plates

$$v'_0 = \frac{v_0 - v}{1 - \frac{v_0 v}{c^2}} = c \frac{\beta_0 - \beta}{1 - \beta_0 \beta} \leftarrow \begin{matrix} \beta_0 = \frac{v_0}{c} \\ \beta = \frac{v}{c} \end{matrix}$$

in fram F' , the charge desity $\sigma' = \frac{\sigma}{\gamma_0} \gamma'_0$, where $\gamma_0 = \frac{1}{\sqrt{1 - \beta_0^2}}$

$$\gamma'_0 = \frac{1}{\sqrt{1 - \left(\frac{\beta_0 - \beta}{1 - \beta_0 \beta}\right)^2}} = \frac{1 - \beta_0 \beta}{\sqrt{(1 - \beta_0^2)(1 - \beta^2)}} \Rightarrow \sigma' = \sigma \frac{1 - \beta_0 \beta}{\sqrt{1 - \beta^2}} = \gamma \sigma (1 - \beta_0 \beta)$$

$$\text{thus } J'_x = \sigma' v'_0 = \gamma \sigma (1 - \beta_0 \beta) v'_0 = \gamma \sigma (\beta_0 - \beta) c$$

$$\Rightarrow E'_y = 4\pi\sigma' = 4\pi\sigma \gamma (1 - \beta_0 \beta) = \gamma \left[4\pi\sigma - \frac{4\pi\sigma v_0}{c} \left(\frac{v}{c}\right) \right]$$

$$B'_z = \frac{4\pi}{c} J'_x = \gamma \left[\frac{4\pi\sigma v_0}{c} - 4\pi\sigma \left(\frac{v}{c}\right) \right]$$

or

$$\begin{aligned} E'_y &= \gamma(E_y - \beta B_z) \\ B'_z &= \gamma(-\beta E_y + B_z) \end{aligned}$$

We can derive the rules for other components: F' is moving at speed of v along the x -direction, respect to F , then.

$$\begin{aligned} E'_x &= E_x, & E'_y &= \gamma(E_y - \beta B_z), & E'_z &= \gamma[E_z + \beta B_y] \\ B'_x &= B_x, & B'_y &= \gamma(B_y + \beta E_z), & B'_z &= \gamma[B_z - \beta E_y] \end{aligned}$$

first order \rightarrow

$$\begin{aligned} \vec{E}' &= \vec{E} + \frac{\vec{v}}{c} \times \vec{B} \\ \vec{B}' &= \vec{B} - \frac{\vec{v}}{c} \times \vec{E} \end{aligned}$$

Suppose in the Frame F , that $B=0, \Rightarrow$

$$\begin{aligned} E'_x &= E_x, & E'_y &= \gamma E_y, & E'_z &= \gamma E_z \\ B'_x &= 0, & B'_y &= \beta \gamma E_z, & B'_z &= -\gamma \beta E_y \end{aligned}$$

then

$$\vec{B}' = -\left(\frac{\vec{v}}{c}\right) \times \vec{E}'$$

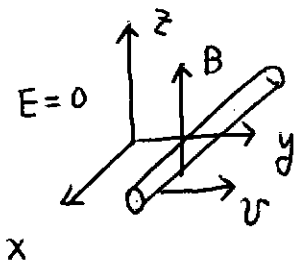
\vec{v} is the velocity of F' respect to F .

Similarly, if in the frame F in which $E=0$, then in the frame F'

we have

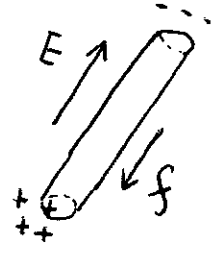
$$\vec{E}' = +\left(\frac{\vec{v}}{c}\right) \times \vec{B}'$$

§ A conducting rod moving in B-field



in the F-frame, $E=0$, $B=B\hat{z}$, the rod is moving along \hat{y} .

Lorentz force $\vec{f} = \frac{q}{c} \vec{v} \times \vec{B}$

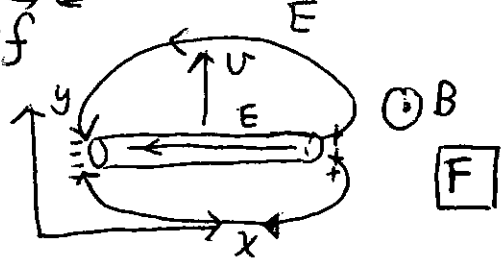


f drives charge accumulate at ends that there's internal electric field

$\Rightarrow q\vec{E} = -\vec{f}$

$\vec{E} = -\frac{1}{c} \vec{v} \times \vec{B}$

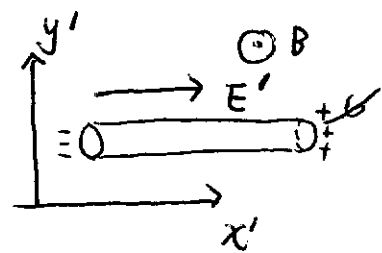
in frame F



Now let us sit the co-moving frame F' with F . For the moment, we neglect the rod, then we will see in the frame F' , there exist B' and E' .

$\vec{B}' \approx \vec{B} - \frac{\vec{v} \times \vec{E}}{c} \approx \vec{B}$ up to β^2 .

$\vec{E}' = \frac{\vec{v}}{c} \times \vec{B}'$



in F' , the rod is at rest. \vec{E}' field

induces charge distributions on the rod. There's no electric field

inside the rod! Thus no motion of electric charge!

