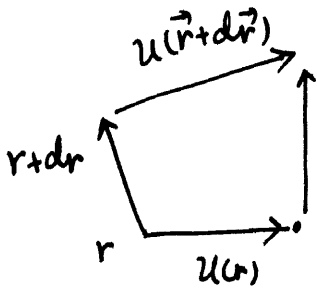


Lect 13. Elasticity of Solids (II)

§ Strain tensor:

Consider a small volume originally at position \vec{r} , but its new position is shifted to $\vec{r} + \vec{u}(r)$. A uniform $\vec{u}(r) = \vec{u}_0$ is just an overall translation, but not distortion. We define the derivative matrix

$$du_i = \sum_j \underbrace{\frac{\partial u_i}{\partial r_j}}_{D_{ij}} dr_j, \quad \text{where } \vec{D} = \begin{bmatrix} \frac{\partial u_1}{\partial r_1} & \dots & \frac{\partial u_1}{\partial r_3} \\ \vdots & & \vdots \\ \frac{\partial u_3}{\partial r_1} & \dots & \frac{\partial u_3}{\partial r_3} \end{bmatrix}$$



How ever, a rotation will cause non-vanishing D_{ij} , but it's not distortion either!

For a rotation

$$d\vec{u}(r) = \vec{v} dt = \vec{\omega} dt \times d\vec{r} = d\vec{\theta} \times \vec{r}$$

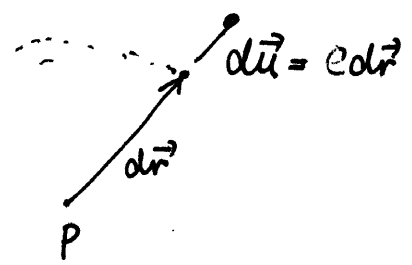
$$D = \begin{bmatrix} 0 & \theta_3 & -\theta_2 \\ -\theta_3 & 0 & \theta_1 \\ \theta_2 & -\theta_1 & 0 \end{bmatrix} \quad \text{which is anti-symmetric.}$$

We decompose D_{ij} into the anti-symmetric part A_{ij} and the symmetric part E_{ij} , where $Z_{ij} = \frac{1}{2} (D_{ij} + D_{ji})$.

symmetric part E_{ij} , where $Z_{ij} = \frac{1}{2} (D_{ij} + D_{ji})$.

Example: dilatation

$E_{ij} = e I$ → trace-part of E_{ij}
 → spherical strain
 dilatation

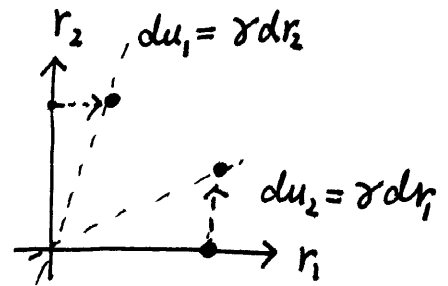


expansion & contraction $\frac{dV}{V} = 3e$ ($e \ll 1$)

Example: Shearing strain — trace-less part (off-d

$E = \begin{bmatrix} 0 & \gamma & 0 \\ \gamma & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$ ($\gamma \ll 1$), $\frac{\partial u_1}{\partial y} = \frac{\partial u_2}{\partial x} = \gamma$

$\begin{bmatrix} 0 & 0 & \gamma \\ 0 & 0 & 0 \\ \gamma & 0 & 0 \end{bmatrix}, \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & \gamma \\ 0 & \gamma & 0 \end{bmatrix}$



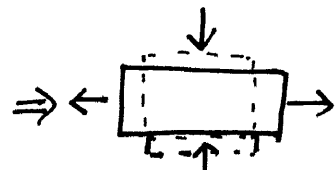
Example:

$\begin{bmatrix} \epsilon_{11} & & \\ & \epsilon_{22} & \\ & & \epsilon_{33} \end{bmatrix}$

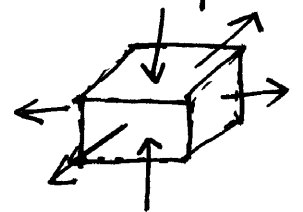
stretching elements:

dilatation: $e = \frac{1}{3} \text{tr} E : \begin{bmatrix} e & & \\ & e & \\ & & e \end{bmatrix}$

$x^2 - y^2 : \begin{bmatrix} \epsilon & 0 & 0 \\ 0 & -\epsilon & 0 \\ 0 & 0 & 0 \end{bmatrix}$



$x^2 + y^2 - 2z^2 : \begin{bmatrix} \epsilon & 0 & 0 \\ 0 & \epsilon & 0 \\ 0 & 0 & -2\epsilon \end{bmatrix}$



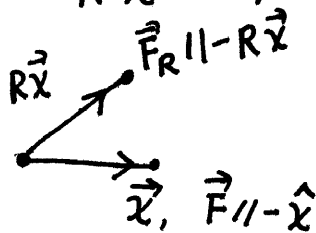
The generalized - Hooke's law

* we want to find the relation between the stress tensor Σ , and the strain tensor. The relation should be linear for small strain, and should be rotationally invariant.

$$\boxed{\Sigma(E_R) = \Sigma_R(E)}, \text{ i.e., the stress of}$$

a rotated strain, should equal to the result of rotating Σ due to the original E .

a simpler example $\vec{F} = -k \vec{x} \Rightarrow \vec{F}(R\vec{x}) = R \vec{F}(\vec{x})$



i.e. the property at $R\vec{x}$ can be obtained by the one at \vec{x} through suitable operation.

result of isotropy of space.

The strain tensor can be decomposed into the trace (spherical)

& the traceless part

$$\vec{E} = e \vec{I} + \vec{E}'$$

\uparrow \uparrow
 (spherical part) (traceless part)

$$\frac{1}{3} (E_{xx} + E_{yy} + E_{zz})$$

5-different components

analogy to 5-d-orbitals

$$\begin{aligned} & \frac{1}{2} (E_{xy} + E_{yx}) & \frac{1}{2} (E_{xx} - E_{yy}) \\ & \frac{1}{2} (E_{xz} + E_{zx}) & \frac{1}{\sqrt{3}} (E_{xx} + E_{yy} - 2E_{zz}) \\ & \frac{1}{2} (E_{yz} + E_{zy}) & \end{aligned}$$

\vec{I} and \vec{E}' transform differently under rotation.

$$\Rightarrow \Sigma = \alpha e I + \beta E' = (\alpha - \beta) e I + \beta E.$$

$$\text{tr } \Sigma = 3\alpha e \Rightarrow e = \frac{\text{tr } \Sigma}{3\alpha}$$

$$\Rightarrow E = \frac{1}{\beta} [\Sigma - (\alpha - \beta) e I] = \frac{1}{\beta} \Sigma - \frac{\alpha - \beta}{3\alpha\beta} (\text{tr } \Sigma) I.$$

* Bulk modulus

$$p = -BM \cdot \frac{dV}{V}$$

$$\Sigma = -p I \Rightarrow \begin{pmatrix} -p & 0 & 0 \\ 0 & -p & 0 \\ 0 & 0 & -p \end{pmatrix}$$

$$E = \frac{1}{\beta} (-p I) - \frac{\alpha - \beta}{3\alpha\beta} (-3p) I \\ = -\frac{p}{\alpha} I$$

$$\Rightarrow e = -\frac{p}{\alpha}$$

$$\frac{dV}{V} = 3e = -\frac{3p}{\alpha}$$

$$\Rightarrow \boxed{BM = \frac{-p}{dV/V} = \frac{-p}{-3p/\alpha} = \frac{\alpha}{3}}$$

* Shear modulus

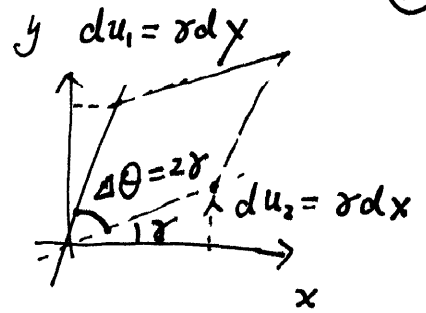
$$\frac{F}{A} = SM \frac{dy}{dx} = SM \cdot \theta$$

consider the case of $e=0 \Rightarrow \Sigma = \beta E$, $\Sigma = \begin{pmatrix} 0 & \sigma_{12} & 0 \\ \sigma_{12} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} = \beta \begin{pmatrix} 0 & \epsilon_{12} & 0 \\ \epsilon_{12} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$

$$\frac{F}{A} = \sigma_{12} = \beta \epsilon_{12} = \beta \gamma$$

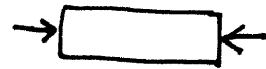
(5)

$$\frac{F}{A} = \beta \sigma = \beta \frac{\theta}{2} = SM \cdot \theta \Rightarrow \beta = 2 SM$$



* Young's modulus

$$YM = \frac{dF/A}{dl/l}$$



$$\Sigma = \begin{bmatrix} \sigma_{11} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \Rightarrow E = \frac{1}{3\alpha\beta} [3\alpha \Sigma + (\beta - \alpha) \text{tr} \Sigma \mathbf{I}] = \frac{\sigma_{11}}{3\alpha\beta} \begin{bmatrix} 2\alpha + \beta & 0 & 0 \\ 0 & \beta - \alpha & 0 \\ 0 & 0 & \beta - \alpha \end{bmatrix}$$

$$dF/A = \sigma_{11}, \quad dl/l = \epsilon_{11} = \frac{\sigma_{11}}{3\alpha\beta} (2\alpha + \beta)$$

$$\Rightarrow YM = \frac{\sigma_{11}}{\sigma_{11} (2\alpha + \beta) / (3\alpha\beta)} = \frac{3\alpha\beta}{2\alpha + \beta} = \frac{9 BM \cdot SM}{3 BM + SM}$$